



Performance of Solar Contribution in Hybrid Parabolic trough Power Plants on Solar Extraction System in Algeria

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Parabolic trough power plants have been developed on several concepts for production of renewable energy in integrated solar combined cycle system (ISCCS) and direct steam generation (DSG). Each concept has their characteristic due to solar energy configuration. Recently, technology for Solar aided power generation (SAPG) is appeared for optimization of these concepts by solar contribution system in hybrid power plants. The aim of this work is thermodynamic analysis on solar hybrid power plants system for ISCCS and DSG concepts. For these concepts, we evaluated the main differences in solar efficiency to electrical power. The solar aided power generation was proposed for evaluating the solar contribution in DSG concept. The study shows that the share of solar contribution in DSG concept is high, for the best method on thermal solar extraction in the DSG concept. Therefore, the optimum value of solar extraction is to preheat the feed water in the heater. These models were evaluated in this work which is simulated on TRNSYS software and System Advisor Model (SAM). The analysis in performance of hybrid concepts and solar contribution in new DSG concept can be evaluated. It was found the best method is solar contribution in the solar hybrid power plants.

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INTRODUCTION

The renewable energy in concentrating solar power is the result of more than fifty years of research and development at universities' laboratories level. Scientists have experimented new approaches to produce electricity via concentrating on solar rays. The rays are diffused in the nature under mild form, so it necessity to concentrate these rays to get high temperature and pressure for electrical power productions. Many concepts for concentration of solar ray were developed. Finally, parabolic trough is the commercial technology.

Algeria is oil state and has a large solar radiation from largest desert in the world. So the New Energy Algeria (NEAL)- has programmed many power projects. The first project is the hybrid natural gas/solar power plant in Hassi R'male at 420 km south of Algiers is in operation since 2011 [1].

The solar power stations with parabolic trough collectors currently account for 94% of the power stations in operation. It is also the technology privileged for the majority of power stations [2]. The parabolic trough systems were implemented for several concentrated solar power (CSP) technologies; actually two concepts for converting solar to electricity first one is the integrated solar combined cycle system (ISCCS) and second is the direct steam generation (DSG). Until now the parabolic trough have several concepts in hybridization to increase their efficiency and continuous generation in dark.

Hybridization means the combination of different energy conversion technologies in one system. Combination between solar-fossil hybrid concept is called integrated solar combined cycle (ISCC), where the solar-produced steam is superheated through a waste heat recovery heat exchanger by the use of heat energy of gas turbine exhaust gas [3]. Therefore, discontinuous

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DSG on different cycle of steam parameters in several configurations for solar contribution.

The target is to simulate and analyse thermodynamic model similar to ISCCS design [22], which is the base of this work. The SAM and TRNSYS software are used to build the concept for each models of hybrid power plants including the gas turbine, steam turbine, HRSG and solar components. Finally, we evaluate the best parameters in output electricity production by featuring this concept in solar contribution.

Model of solar hybrid power plants

The model selected for simulation based on hybrid station (ISCCS) design Hassi R'male [22] which includes Heat Transfer Fluid (HTF), with actual operational condition takes into account the weather and the region. This reference plant is located at the south of Algeria in Hassi R'male, province of Laghouat at about 500 km from Algiers. The solar in hot period with Direct Normal irradiation (DNI) can reach to 930 W/m².

The solar power plant include the solar field and power block. The power block in conventional combined cycle power plant with two gas turbine on 47 MW SGT-800 in Brayton cycle [22], incorporated with Rankin cycle for a steam turbine on SST-900 [24]. The solar field for 183120 m² comprises 224 parabolic collectors assembled in 56 loops, 4 collectors per loop and the HTF is the oil, it runs with PTR-70 receivers.

These power plants are modelled and simulated in two commercial codes the SAM [26] and the TRNSYS [27] with a model library STEC developed by DLR; which was used to model the solar components. The design parameters of the each solar power plants are summarized in Table 1.

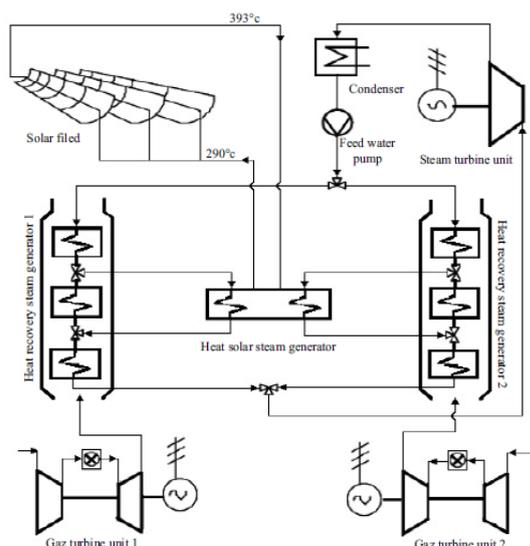


Figure 3. HTF-ISCCS of Hassi R'mmel power plant with simple pressure level [22].

Configuration of the DSG concept in solar contribution system

The component of new concept DSG proposed in configuration is similar to the solar hybrid power plants of Hassi R'male, without Solar Steam Generator and include the receivers for parabolic trough kind PTR-80. This concept is referred for validation of results in solar size initially to produce 200 MW [38].

Two gas turbine units on 47 MW SGT-800 to provide a necessary flexibility in the operation in the night and cloudy day [23]. The steam turbine on SST-900 [24] and the system of heat exchanger include concept that are two heat recovery steam generator (HRSG) to generate steam and gas-boiled for thermodynamic cycle [25].

Table 1. The parameters for each concept DSG and ISCCS

Production	ISCCS	DSG
Gas turbine		
Ambient temperature	35°C	35°
Compressor pressure ratio	20.2	20.2
Compressor isentropic efficiency	0.88	0.88
Inlet turbine temperature	1200°C	1200°C
Turbine isentropic efficiency	0.88	0.88
Exhaust mass flow rate	120, 20 kg/s	120, 20 kg/s
Exhaust temperature	550 °C	550°C
LHV of natural gas	45778 kJ/kg	45778 kJ/kg
Gas natural mass flow rate	2.46 kg/s	2.46 kg/s
Steam turbine		
Inlet steam temperature	500°C	550°C
Inlet steam pressure	83 bars	120 bars
Steam mass flow rate	70 kg/s	70 kg/s
Condensate temperature	52°C	52°C
Isentropic efficiency	0.9	0.9
HRSG		
Fuel mass flow rate	0.66 kg/s	0.66 kg/s
Approach temperature	25°C	25°C
Pressure losses	16 bars	16 bars
Inlet water temperature	60°C	60°C
Thermal efficiency	98.50%	98.50%
Solar Steam Generator		
Inlet water temperature	195°C	-
Inlet water pressure	90 bars	-
Water/steam mass flow rate	22.60 kg/s	-
Pressure losses	5.8 bars	-
Thermal efficiency	98 %	-
Parabolic trough		
Area collector	183120 m ²	-
Heat transfer fluid	PTR-70	-
The receivers type	PTR-80	-
Outlet steam temperature	550°C	-
Outlet receivers pressure	-	-
Outlet HTF temperature	392°C	-
HTF mass flow rate	205 kg/s	-
Water/steam mass flow rate	55 kg/s	-

The new model of DSG concept proposed include the grid of solar field in receivers PTR-80 which is composed of two parts preheater and superheated; these parts load the water or steam, the model is presented in Fig. 4. In the new DSG concept, liquid water from the deaerator is pumped to the proper pressure levels for to feed the feed water heater, at same times preheated on

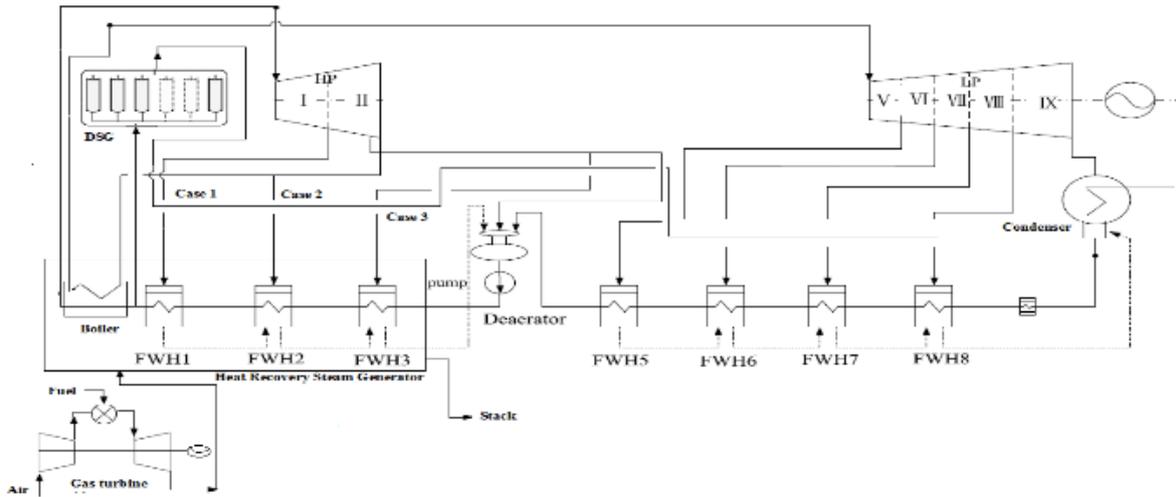


Figure 4. Schematic diagram of a solar contribution on DSG concept, in which solar thermal energy used to preheat the feed water heater.

the first DSG solar field in the saturated case, and then vaporized in the second DSG solar field in superheated case (the solar field is not described in diagram below). When wet steam produced from the solar collectors it separated in a vacuum, the liquid returns to the solar fields, saturated steam is superheated by the gas turbine exhaust gas in HRSG before heading to the steam turbine. After high-pressure stage turbine, the steam returns to HRSG, to be reheated and feeds the next stage steam turbine.

The new DSG concept in configurations for simulation are presented in subsystems, each subsystem include extraction point from solar field to heat the feedwater which is fed the DSG solar field. In this new concept DSG the feedwater is heated by solar thermal energy carried from parabolic trough; but there is a large loss of exergy. The exergy loss in the heaters can be reduced by increasing the number of extraction stages (and feedwater heaters), so we simulate the best approach for extraction in order to get the best performance efficiency.

Analyses for combined cycle system

The following model is evaluation for thermodynamic analyse of the solar integration system in each configuration. We use the first law of thermodynamics energy balance form should be used for control volume [28]:

$$\frac{dE_{cv}}{dt} = \sum \dot{m}_i \left(h_i + \frac{v_i^2}{2} + gz_i \right) - \sum \dot{m}_o \left(h_o + \frac{v_o^2}{2} + gz_o \right) + \dot{Q}_{cv} - \dot{W}_{cv} \quad (1)$$

The thermodynamic process in a steam turbine is an isentropic transformation. The ideal outlet steam specific

enthalpy can be obtained from steam tables because the outlet steam pressure and steam entropy are known. For exergy balance in a control volume, the following equation has been used [28]:

$$\sum \dot{Q}_r + \sum \dot{m}_i \left(h_i + \frac{v_i^2}{2} + gz_i \right) = \frac{dE_{cs}}{dt} + \sum \dot{m}_o \left(h_o + \frac{v_o^2}{2} + gz_o \right) + \dot{W} \quad (2)$$

The control volume for irreversibility explanation, in the following equation is used [30]:

$$\dot{I}_{cv} = \left(\sum \dot{m}_i \psi_i - \sum \dot{m}_o \psi_o \right) + \sum \left(1 - \frac{T_0}{T} \right) \dot{Q}_{cv} - \dot{W}_{cv} \quad (3)$$

In exergy calculation of all cycle equipment, we should calculate all exergy flows. The exergy calculation for single-phase flows such as water or steam flow is easily carried out. For this action following relevance is used [28]:

$$\psi = (h - h_0) - T_0(s - s_0) \quad (4)$$

For transferred exergy by heat [30]:

$$\psi_Q = Q \left(1 - \frac{T_0}{T} \right) \quad (5)$$

Efficiency of collector receiver for solar field

The DSG plant use the PTR-80 receivers because of higher temperature and pressure (550C° and 120 bars) in recirculation mode as well as to minimize pressure drop over the collector loop.

The ISCCS plant use the PTR-70 receivers are commercialized in worldwide. At this step, we have chosen Algeria area with Tamanrasset city, other worth the area of Tamanrasset is the hot area in Algeria with direct normal irradiation 2600 kWh/m²/ year .

The simulation model for the parabolic trough collectors using water-steam as heat transfer fluid, has already been developed and validated in other work [31]. Another model for the parabolic trough, their cycle is activated in a central water boiler heated by the oil coming from the solar field [30].

The efficiency of collector η_{col} is given by the Hottel-Whillier Bliss equation [11], it is defined as;

$$\eta_{col} = \frac{Q_{col,net}}{DNI \cdot A_{col}} \quad (6)$$

$Q_{col,net}$ (kWth) is the net heat gain per collector loop is the energy balance applied to the troughs; it allows the calculation of the thermal power transferred to the fluid as a function of the impinging Direct Normal Irradiation (DNI) on the tube is defined as follows;

$$Q_{col,net} = [[DNI \cdot f \rho \alpha] - [U_A (T_b - T_m) / C] - [\varepsilon \sigma (T_b^4 - T_m^4) / C]] \cdot A_{col} \quad (7)$$

where η_{col} is the collector efficiency; DNI (kWth) is the incident direct normal irradiation to the collector aperture area.

- A_{col} (m²) is the total collector area of the solar field.
- ρ is the reflection coefficient of mirror 0.85.
- α is the absorption coefficient of pipe 0.96.
- U_A is the heat transmission index of the absorber 8W/m² K.
- T_b is the absorber temperature (K).
- T_m is the ambient temperature (K).
- ε is the emission coefficient of the absorber 0.15, σ is the Stefan-Boltzmann constant (5.67*10⁻⁸/m²K⁴).
- $C = A_r/A_a = 60$ is the concentration ratio with A_r aperture area and A_a absorber area [32].
- The factor f is a multiplication coefficient to reduce the η_{col} of series parallel connected collectors as its efficiency is smaller than that for single collector where 0.85< f <0.95 [33].

Efficiency of isccs and dsq power plant

The solar thermal energy of the cycle concept of DSG and ISCCS systems is defined as follows:

$$Q_{sol-el} = Q_{ccs} - \dot{m}_{ff} * LHV_{ff} \quad (8)$$

where:

Q_{ccs} is the thermal energy of output the combined cycle system (kWth). (\dot{m})_{ff} is the mass flow rate of the fuel

consumed in the gas turbine. $[LHV]_{ff}$ is the fuel's lower heating value from gas turbine.

To evaluate the cycle efficiency, we need to evaluate the electric power coming from the solar source and determine the thermal energy of the cycle, so this fraction between solar and combined cycle is the solar-to-electrical efficiency are defined as follows:

$$\eta_{sol-el} = \frac{Q_{sol-el}}{DNI * A_{col}} \quad (9)$$

All previous work estimated that the coal-fired power plants are operating in the regenerative Rankine cycle. In a typical regenerative Rankine cycle power plant, some steam is extracted from the turbine to preheat the boiler feedwater, which can increase the overall thermal efficiency of the plant [34]. When the extracted steam partly or totally replaced by solar thermal energy carried by heat transfer fluid to preheat the feedwater, this operation is solar contribution in hybrid power plant.

Analyses the solar contribution in dsq concept

The solar aided power generation (SAPG) concept, is to use solar thermal energy to replace the bled-off steam in regenerative Rankine power cycle. This extracted bled off steam is normally used to preheat feed water entering the boiler; it has the effect of increasing the thermal efficiency of the cycle [35, 36].

$$\eta_{th} = \frac{W_{net}}{Q_{ff} + Q_{sol,net}} = \frac{W_{net}}{m_{ff} * LHV + Q_{sol,net}} \quad (10)$$

where W_{net} is the system's total net power output including both from gas turbine and steam turbines, Q_f is the thermal energy provided from the fuel which is equal to the mass flow rate of the fuel m_{ff} consumed multiplies the fuel's lower heating value (LHV), $Q_{sol,net}$ is the absorbed solar heat by water/steam.

The exergy efficiency is also calculated for the system performance evaluation. Assuming that methane's chemical exergy is approximately equal to 1.04 times its LHV, and the solar thermal exergy corresponds to the maximal work availability between solar collector temperature (T_{sol}) and ambient temperature (T_0), so the definition of system exergy efficiency is given as follows [37] :

$$\eta_{ex} = \frac{W_{net}}{Q_{ff,ex} + Q_{sol,net} \left(1 - \frac{T_0}{T_{sol}}\right)} = \frac{W_{net}}{1.04 m_{ff} * LHV + Q_{sol,net} \left(1 - \frac{T_0}{T_{sol}}\right)} \quad (11)$$

The steam cycle thermal efficiency η_{steam} is defined as the ratio of steam turbine power output W_{steam} to the total thermal input to the steam cycle from solar field Q_{sol} and gas turbine exhaust Q_{exh} :

$$\eta_{steam} = \frac{W_{steam}}{Q_{sol,net} + Q_{exh}} \quad (12)$$

The contribution of the solar heat in the total heating load can be measured by its share in the system's total heat input:

$$X_{sol} = \frac{Q_{sol,net}}{Q_{ff} + Q_{sol,net}} = \frac{Q_{sol,net}}{m_{ff} * LHV + Q_{sol,net}} \quad (13)$$

The fossil fuel could be saved if the plant's power output remains unchanged as the same as the reference CCGT plant. The fossil fuel saving levels in comparison with the reference CCGT plant, for the same amount of electricity generated, is termed as the fossil fuel saving ratio:

$$SR_f = \frac{Q_{ccs} - Q_f}{Q_{ccs}} \quad (14)$$

RESULTS AND DISCUSSION

Analyses the performance in hybrid concept model

Firstly we calculate the total annual net heat gain per collector loop, other word the heat output by solar collector in each concept for the power plant introduced in Fig. 4.

For different months in each power plants, there are variations in solar field performance, the solar field output $Q_{col,net}$ increase according the solar radiation in each month until season of the summer when it has reached to the peak, due a high radiation and the solar field decrease when the summer is over, as well as there are variations between the DSG and the ISCCS due a heat transfer fluid. In the annual simulation for one years the output of solar field is varied in each concept. The DSG concept use water like as a heat transfer fluid and it has reached to 500 C° and 120 bar, the peak value of output solar field at midday is 138 MWth, while the ISCCS use oil (Therminol VP-1) as like as heat transfer fluid and it has reached to 400 C° and the peak value at midday is 124 MWth.

We determine the increase effect of the direct normal irradiation (DNI) in the efficiency of collector loop η_{col} for each integrated power plant and the results of simulation are presented in Fig. 5.

The receiver tube efficiency increase when the DNI increase. The DSG systems include only steam in high temperature, but in ISCCS the receiver include only oil, thereby the steam is more efficiency than the oil in heat transfer, the steam reach to the efficiency for 67%, but the oil concept cannot be reached to 63% (see Fig. 6). For this reason oil and steam have variation in efficiencies η_{col} . It can be seen that the ISCCS reaches to the value of 400 C° and 80 bar, this characteristic is from the

propriety chemical, while in the DSG concept the values reached is 500C° and 120 bar. Therefore the efficiency in the HTF system is less than DSG concept is depending from the heat transfer fluids in receiver tube.

The ISCCS and DSG plants has been taken into account one-year period to determine the annual performance for both concepts, as well as this simulation is analysed in day light when the sunrise until sunset. Table 2 shows the overall annual power production. The cycle of each power plant is analysed and simulates the solar-to-electric efficiency of the DSG and ISCCS is shown in the following chart.

The several behaviour of the analysed solar collector technologies is evident in the first estimation. The simulation explain that the DSG and ISCCS are able to have a very high efficiency in summer months, due to high percent of DNI in this months, whilst efficiency of DSG is 6 % more than ISCCS, this variation is from the kind of heat transfer fluid in receiver tube.

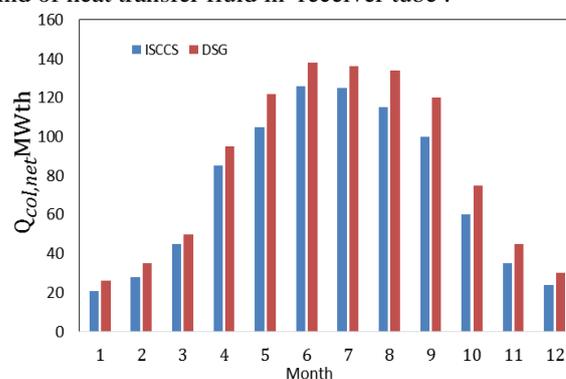


Figure 5. The monthly power of solar field output in DSG and ISCCS

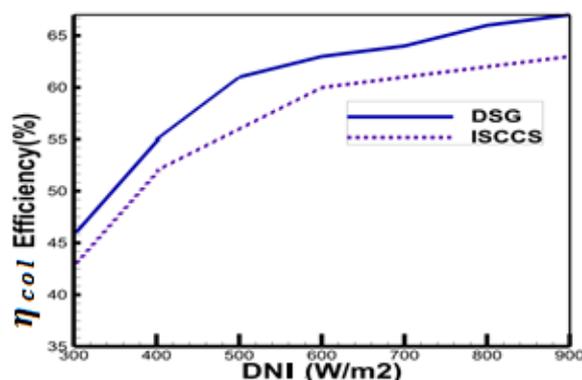


Figure 6. The effect of direct normal radiation in DSG and ISCCS

Conversely in winter the efficiency decays of the solar energy in both concept DSG and ISCCS, this variation lead to decrease in solar to electric efficiency, with less than 3% of difference between each concept (see Fig. 7).

The annual electricity production and annual natural gas consumption have been calculated in Table 2 taking into account the monthly percentage of clear cloudy and overcast days.

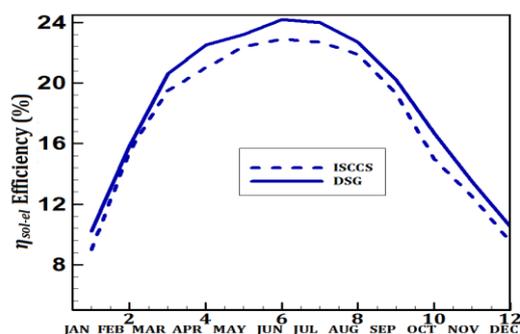


Figure 7. The monthly efficiency power solar-to-electric

TABLE 2. The production solar combined system plant performance

Plant type	ISCCS plant	DSG plant
Gas turbine	47 MW	47 MW
Steam turbine	80 MW	80MW
Parabolic trough	30MW	36MW
Annual gas consumptio	20845.43 m ³	12548.67 m ³
Gas percentage in electricity at day light	13.6%	8.7%

When comparing the ISCCS and the DSG plant, it can be concluded that DSG work better than ISCCS this behaviour due of cloudy and overcast day, so the gas turbine is operated for balance the shortage in heat losses as well as more fuel consumption (Table 2).

Analyse the performance for solar contribution in DSG concept

Previous work in the hybrid power plants based on evaluation of the HTF for solar contribution when the oil is the HTF. In this study, for analyse the DSG concept we take on compete the water and steam in DSG system. The new model proposed is validated according to literature [38]. We assumed that the DSG concept for simulation, that the cycle include two stage steam turbine in three extraction point from solar field to heat the feedwater.

The extraction steam is from solar thermal energy carried by parabolic trough, including steam or vapour saturated for to preheat the feedwater shown in Fig. 4. We assumed the amount of steam in every extraction point from parabolic trough is the same with high-pressure (superheated solar field). So, sufficient heat to raise the feedwater temperature (FWH 1, FWH 2, FWH 3), every extraction is one case, the first one scenario case 1 is the configuration with extraction from the superheated solar field, the output steam leaving the solar

field is directly preheat the feed water FWH1. The second configuration case 2 with extractions the steam from the superheated solar field to preheat feed water FWH2.

The final scenario case 3 which include the extraction of steam from parabolic trough to preheat the FWH3. Therefore, there are three cases for the model analysed.

Firstly we determined the best case in analyse thermodynamic for all parameters, secondly we compared the solar contribution on best case simulated to the best case results given in literature [38]. According the analyses and simulation of the model in each case on the TRNSYS software, the results are in the table below. The results of this simulation showed the best share of solar contribution in the hybrid power plant, when we preheat the feed water we decrease losses of solar thermal energy, despite the legend decrease in thermal efficiency. Case 1 is the best way to preheat the feed water with $X_{sol}=29.2\%$, almost the best approach to preheat the last feed water near the boiler (see Fig. 8).

Finally we compared the best concept simulated when we used the new DSG concept in effect of solar contribution to the results reported in literature [38].

The solar contribution is varied in each concept, it can be seen that the new DSG concept have a large share solar in electric production, with the effect of best way for to reheat the feed water and decrease the losses. The annual solar to power efficiency in each concept increase when the solar collector area increase until a peak value 29% in the efficiency and 170000 m² of solar collector area, than the efficiency decrease when the solar collector area increase due for more losses to collect all collector area in parabolic trough (see Fig. 9).

The new concept DSG has high output solar thermal energy it can be reached to 118GWh, but the reference HTF concept not exceeded the value 114GWh in same collector area to new DSG concept. Hence, more solar collector area more solar output and more losses. Furthermore the DSG concept show their performance in the solar contribution.

According to these simulation of the solar contribution in new DSG concept proposed, the output power increase when we preheat the last feed water from the superheated

TABLE 3. Performance for solar contribution

Items	Case1	Case2	Case3
Solar heat input, $Q_{sol,net}$ (MW)	96	84	73
Solar thermal share, X_{sol} (%)	29.2	26.5	24
Fossil fuel saving ratio, SR_f (%)	29.5	26.7	24.2
Net power output, W_{net} (MW)	168	164	160
System thermal efficiency, η_{th} (%)	51.2	51.8	52.4
Steam cycle thermal efficiency $\eta_{steam}(\%)$	26.5	26.2	26.
System exergy efficiency η_{ex} (%)	52.1	52.9	53.3

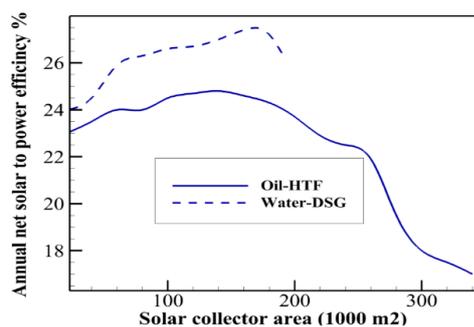


Figure 8. The annual net solar to power efficiency in solar contribution method

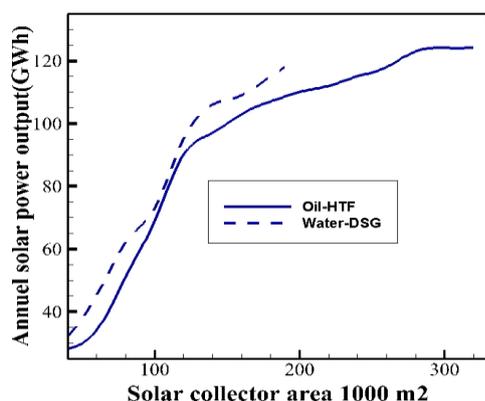


Figure 9. The annual solar power output in solar contribution method

parabolic trough ,other words to heat the last feed water it mean less losses in heat and short way to feed the steam turbine . Furthermore the best approach to increase efficiency is to decrease the losses.

CONCLUSION

The influence of the solar on the annual performance of direct steam generation and integrated solar combined cycle system is detailed whose system analysis has been performed .The DSG plants proves the height efficiency after the development of new receiver as well as solve the trouble for pressure drop in recirculation mode, and the ISCCS plant until recent use of complex heat transfer system in the process and low efficiency. Therefore, the result in this study indicate that ;the DSG plant in annual production is 4 % higher than the ISCCS power plant in same design and area condition of Algeria desert .

The DSG concept in solar contribution mode with the simulated results showed that; the extraction of solar thermal to preheat the last feed water behind the boiler, is the best performance compared to HTF concept .The efficiency of solar production has reached 29%.We conclude that the effect of solar contribution is to decrease losses of energy. Therefore, increase efficiency in solar to electric performance .

These results are a detail performance of the

parabolic trough solar thermal power plants in the DSG and HTF. This work is not taken into the economic study. This step is remained a critical point in the development of solar parabolic trough plant.

REFERENCES

1. David. Kearney & Associates. Vashon, Washington, National Renewable Energy Laboratory (NREL). Subcontract And Reviewed By Guidelines (April 2009, December 2010).
2. Syndicat des énergies renouvelables Les fiches d'informations sur l'énergie solaire thermodynamique, Principe of operation of thermodynamic, www.enr.fr. Accessed on May2010.
3. Allani Y. CO2 mitigation through the use of hybrid solar-combined cycles. Energy Conversion Management (1997), 38, S661-S7.
4. Kuenstle, K, Lezuo, A., Reiter, K. Solar powered combined cycle. Proceedings of the Power Gen Europe '94, Cologne, 1994 17-19May.
5. Steinmann, W.-D., Eck, M., Direct solar steam generation in parabolic troughs. Proceedings of the 10th Solar PACES International Symposium on Solar Thermal Concentrating Technologies, Sydney 2000., pp. 107-112.
6. Zhai RR, Yang YP, Zhu Y, et al. The evaluation of solar contribution in solaraided coal-fired power plant. Int J Photoenergy 2013.
7. Hou H, Xu Z, Yang Y. An evaluation method of solar contribution in a solar aided power generation (SAPG) system based on exergy analysis. Appl Energy 2016;182:1-8.
8. Johansson .TB, et al., editors. Renewable Energy, Sources for Fuels and Electricity. Washington, DC: Island Press (1993) , P. 234-5.
9. Kelly, B., Herrmann, U., Hale, M.J. Optimization Studies for Integrated Solar Combined Cycle Systems. Proceedings Of Solar Forum 2001 - Solar Energy: The Power To Choose, Washington.
10. Status Report on Solar Trough Power Plants. Sponsored by the German Federal Minister for Education, Science, Research and Technology under Contract No (1996). 0329660.P 40, 56.
11. Solar Engineering of Thermal Process. Wiliam A.Bickman. John A.Duffie (2013). Simulation in solar process design
12. McMahan A, Zervos N. Integrating steam generation from concentrating solar thermal collectors to displace duct burner fuel in combined cycle power plants. In: Power-Gen International 2009. Las Vegas.
13. Montes, M.J. et al. Thermo Fluid Dynamic Model and Comparative Analysis of Parabolic Trough Collectors Using Oil, Water/Steam or Molten Salt as Heat Transfer Fluids. In Proceedings of 14th International Solar PACES Symposium on Solar Thermal Concentrating Technologies, Las Vegas, USA (2008).
14. Benz, N. et al. Advances in Receiver Technology for Parabolic Troughs. Proceedings of 14th International Solar PACES Symposium on Solar Thermal Concentrating Technologies, Las Vegas, USA (2008) .
15. Zarza E., Valenzuela L., et al. Direct Steam Generation in Parabolic Troughs: Final Results and Conclusions of the DISS Project. Energy (2004) , 29 (5), 635-644.
16. Krüger D. Krüger J., et al. Kanchanaburi Solar Thermal Power Plant with Direct Steam Generation – Layout. Proceedings of the 16th CSP Solar PACES Symposium, Perpignan, France (2010)..
17. Eck M., Benz N., et al. The Potential of Direct Steam Generation in Parabolic Troughs - Results of the German Project DIVA. Proceedings of the 14th Biennial CSP Solar PACES Symposium, Las Vegas, USA (2008).

18. Price H., Luffert E., et al. Advances in Parabolic Trough Solar Power Technology. *Journal of Solar Energy Engineering*, (2002) 124(2), 109-125.
19. Zarza E.) DISS Phase II Final Report. EU Contract No (2002). JOR3-CT98-0277.
20. Omar Behara, Abdallah Kellaf, et al., Instantaneous performance of the first Integrated Solar Combined Cycle System in Algeria. *MEDGREEN 2011-LB.Energy Procedia* 6 (2011) 185-193.
21. Eck, M. and Hirsch, T. Dynamics and control of parabolic trough collector loops with direct steam generation, *Solar Energy* (February 2007), 81(2), 268-279.
22. Fouad Khaldi, Energy and exergy analysis of the first hybrid solar-gas power plant in Algeria. *Proceedings of ECOS 2012 - The 25th International Conference on Efficiency, Cost, Optimization, Simulation and Environmental Impact of Energy Systems* June 26-29, 2012, Perugia, Italy.
23. Shukin S., Annerfeldt M. et al. Siemens SGT-800 industrial gas turbine enhanced to 47MW. Design modifications and operation experience. *Power for Land, Sea and Air GT2008*; 2008 Jun 9-13; Berlin, Germany. *Proceedings of ASME*: 65-70.
24. Steam turbines for solar thermal power plants. Siemens AG(2008). Order No. E50001-W410- A105-V1-4A00. Available at <<http://www.siemens.com/energy>> [accessed 12.6.2011].
25. O. Behar, A. Khellaf, K. Mohammedi, S. Ait-Kaci a Review of Integrated Solar Combined Cycle System (ISCCS) with a Parabolic Trough Technology, *Renewable and Sustainable Energy Reviews* . (November 2014), 39, 223-250.
26. Solar Advisor Model (SAM) software .User guide version 2016.03.14. National Renewable Energy Laboratory.
27. Trnsys 17. (2010) <<http://sel.me.wisc.edu/trnsys/>>.
28. Borgnakke C, richard ES. *Fundamentals of thermodynamics*. United State: John Wiley & Sons, Inc; 2009.
29. Frier, S.D., Cohen, G.E., Cable, R.G., An overview of the Kramer Junction parabolic trough solar electric system. In: *Proceeding of ANZSES 36th Annual Conference* Christchurch, New Zealand, (1998) .547-554
30. Montes MJ, Abánades A, Martínez-Val JM. Performance of a direct steam generation solar thermal power plant for electricity production as a function of the solar multiple. *Solar Energy* (2009) , 83,679-89
31. Ahmadi GhR, Toghraie D. Parallel feed water heating repowering of a 200 MW steam power plant. *J Power Technol* 2015;95(4):288-301.
32. Steinmann, W.-D., Eck, M., Direct solar steam generation in parabolic troughs. *Proceedings of the 10th Solar PACES International Symposium on Solar Thermal Concentrating Technologies*, Sydney (2000), pp. 107-112.
33. Kleeman, M., Meliss, M., *Regenerative Energiequellen*. Springer, Berlin, Heidelberg (1988).
34. Hou H, Wu J, Yang Y, et al. Performance of a solar aided power plant in fuel saving mode. *Appl Energy* 2015;160:873-81.
35. Eric . Hu, YongPing Yang, et al. Solar thermal aided power generation. *Applied Energy* 87 (2010) .
36. Yongping Yang a, Qin Yan, et al .An efficient way to use medium-or-low temperature solar heat for power generation e integration into conventional power plant *Applied Thermal Engineering* 31 (2011) 157-162.
37. Yuanyuan Li, Yongping Yang .Thermodynamic analysis of a novel integrated solar combined cycle. *Applied Energy* 122 (2014) 133-142.
38. Jiyun Qin, Eric Huf, Graham J. Nathan. Impact of the operation of non-displaced feedwater heaters on the performance of Solar Aided Power Generation plants. *Energy Conversion and Management* 135 (2017) 1-8.

Persian Abstract

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چکیده

نیروگاه‌های پارابولیک بر روی چندین مفاهیم برای تولید انرژی تجدید پذیر در سیستم ترکیبی جامد خورشیدی (ISCCS) و تولید بخار مستقیم (DSG) توسعه یافته است. هر مفهوم به دلیل پیکربندی انرژی خورشیدی، ویژگی خاصی دارد. به تازگی، تکنولوژی تولید انرژی خورشیدی (SAPG) برای بهینه سازی این مفاهیم با استفاده از سیستم پاداش خورشیدی در نیروگاه های هیبریدی ظاهر می شود. هدف از این کار تجزیه و تحلیل ترمودینامیکی در سیستم نیروگاه های هیبریدی خورشیدی برای مفاهیم ISCCS و DSG است. برای این مفاهیم، تفاوت عمده ای را در بازده خورشیدی به قدرت الکتریکی ارزیابی کردیم. تولید انرژی خورشیدی به منظور ارزیابی مشارکت خورشیدی در مفهوم DSG پیشنهاد شد. این مطالعه نشان می دهد که سهم انرژی خورشیدی در مفهوم DSG برای بهترین روش در استخراج خورشیدی خورشیدی در مفهوم DSG بالا است. بنابراین، مقدار مطلوب استخراج خورشیدی، پیش گرم کردن آب خوراک در بخاری است. این مدل ها در این کار مورد بررسی قرار گرفتند که در نرم افزار TRNSYS و مدل مشاور (SAM) شبیه سازی شده است. تجزیه و تحلیل در عملکرد مفاهیم هیبرید و مشارکت خورشیدی در مفهوم جدید DSG می تواند مورد بررسی قرار گیرد. بهترین روش این بود که کمک خورشیدی در نیروگاه های هیبریدی خورشیدی باشد.
